

TRANSMITTER IDENTIFICATION SYSTEM**CROSS-REFERENCE TO RELATED APPLICATIONS**

[01] The present application claims priority from United States Patent Application No. 60/443,550 filed January 30, 2003.

5 TECHNICAL FIELD

[02] The present invention relates to a transmitter identification system, and in particular to a digital television (DTV) transmitter identification system for identifying the origin of a received DTV signal, which can be used for tuning a distributed-transmission (single-frequency) DTV network, geographic locating, estimating the channel impulse response for a particular transmitter
10 with a very long delay spread capacity, and transmitting robust low bit rate control information to mobile and stationary terminals.

BACKGROUND OF THE INVENTION

[03] Digital television (DTV) networks are comprised of a plurality of transmitters, each broadcasting the same signal using multiple frequencies or a single frequency (single frequency
15 network). As the number of transmitters grows, there is an increased desire to be able to identify the transmitter of origin for each signal received. Transmitter identification will enable broadcasting authorities to identify illegal or improperly operating transmitters. Moreover, transmitter identification can also be used to tune various transmitters in a single frequency network to minimize the effects of multi-path interference. Multi-path interference is caused by the destructive
20 interference of several different transmissions originating from different transmitters and/or caused by the reflection of transmissions. Figure 1 illustrates a single-frequency digital-television network 1, including three transmitters 2, 3 and 4 with transmission ranges 6, 7 and 8, respectively. With reference to the overlap area, designated by reference numeral 9, a receiver positioned therein would receive a transmitted signal comprised of direct transmitted signals 12, 13 and 14 from transmitters 2,
25 3 and 4, respectively, plus reflected transmitted signal 16 from transmitter 2. The reflected transmitted signal 16 resulting from a reflection off of a large obstacle 17, e.g. a large building. Unfortunately, the various components of the transmitted signal may not all be in phase, resulting in undesired effects. The effects of multi-path interference to DTV signals include a degradation in the television picture and sound. In analog television, multi-path interference causes "ghost" images.

[04] United States Patents Nos. 6,075,823 issued June 13, 2000 to Hideaki Sonoda; 6,122,015 issued September 19, 2000 to Al-Dhahir et al; 6,128,337 issued October 3, 2000 to Schipper et al; 6,304,299 issued October 16, 2001 to Frey et al; 6,437,832 issued August 20, 2002 to Grabb et al; and 6,501,804 issued December 31, 2000 issued to Rudolph et al disclose various solutions to overcoming the problem of multi-path interference. In general, the systems disclosed in the aforementioned references compare a transmitted test signal including noise with a reference signal, and construct a filter in accordance with the results of the comparison to remove noise from transmitted digital television signals. Unfortunately, none of the prior art references provide an identification signal for each transmitter, nor do they provide a system for tuning the entire network. Each of the aforementioned systems requires a complicated filtering circuit to be installed in every receiver in the system, which greatly increase the cost to the operator, and therefore the consumer.

[05] An object of the present invention is to overcome the shortcomings of the prior art by providing a transmitter identification system that can be used to identify the transmissions, direct or redirected, from various transmitters.

[06] Another object of the present invention is to provide timing information relating to the transmissions from known transmitters, which can be used to tune the transmitters in a network to minimize the effects of multi-path interference.

SUMMARY OF THE INVENTION

[07] Accordingly, the present invention relates to a method of identifying a transmitter in a distributed digital television transmission network, including a plurality of transmitters and a plurality of receivers, comprising the steps of:

[08] a) providing a signal to be transmitted to each transmitter;

[09] b) embedding an identification sequence into the signal, indicative of the transmitter of origin, forming a combined transmission; and

[10] c) transmitting the combined transmission from each transmitter.

BRIEF DESCRIPTION OF THE DRAWINGS

[11] The invention will be described in greater detail with reference to the accompanying drawings which represent preferred embodiments thereof, wherein:

- [12] Figure 1 is a schematic illustration of a conventional Digital Television Network;
- [13] Figure 2 illustrates a DTV signal frame structure including an identification sequence x_i synchronized therein;
- [14] Figure 3 illustrates a 16-bit Kasami sequence generator;
- 5 [15] Figure 4 illustrates a ATSC signal data field;
- [16] Figure 5 illustrates an auto-correlation function of a 16-bit Kasami sequence;
- [17] Figure 6a illustrates a cross-correlation function over a single segment;
- [18] Figure 6b illustrates a cross-correlation function averaged over 60 segments;
- [19] Figure 7 illustrates an impulse in a cross-correlation function; and
- 10 [20] Figure 8 illustrates an impulse in the cross-correlation function after side-lobe filtering.

DETAILED DESCRIPTION

- [21] In accordance with the present invention, the transmitter identification system embeds an identification sequence in the form of a pseudo-random sequence $x_i(n)$, selected from a set of
 15 orthogonal sequences, in band into each DTV signal $d_i(n)$ creating a combined transmission $d_i'(n)$. In practice, the sequences will be truncated and, therefore, not be perfectly orthogonal; however, for the purposes of the invention they will only need to have negligible cross correlation. Accordingly, orthogonal, substantially-orthogonal and having negligible cross correlation will be used interchangeably so as not to limit the scope of protection to perfectly orthogonal.

- 20 [22] The process is represented by the equation:

$$[23] \quad d_i'(n) = d_i(n) + \rho x_i(n) \quad (1)$$

- [24] wherein ρ represents a gain coefficient controlling the embedding level of the identification sequence, which varies from transmitter to transmitter depending on the modulation and

channel coding schemes of the individual transmitters. After passing through a transmission channel h_i , a transmitted signal r_i from the i^{th} transmitter can be formulated as:

$$[25] \quad r_i(n) = d_i'(n) \otimes h_i + n_i(n) \quad (2)$$

[26] where $n_i(n)$ is the noise for the i -th transmitter.

5 [27] The overall transmitted signal $r(n)$ can be formulated as:

$$[28] \quad r(n) = \sum_{i=1}^M [d_i'(n) \otimes h_i + n_i(n)] \quad (3)$$

[29] Identification of a particular transmitter is impossible without additional identification processes. According to the present invention, details of the existence of a specific transmitter and the strength of each transmitted signal $r_i(n)$ at the reception site can be determined by calculating correlating functions. For example, the correlation between $r(n)$ and a locally generated identification signal $x_j(n)$ can provide identifying information, i.e. existence and strength of the signal, about the j -th transmitter. If a signal from the j -th transmitter is present, i.e. the transmitted signal $r(n)$ contains the identification sequence $x_i(n)$ matching the locally generated sequence $x_j(n)$, an impulse will appear in the cross correlation function (see Figure 5). If more than one impulse is found for a given sequence, the impulse separations are indicative of a multi-path delay. Accordingly, this method can be used in obtaining the impulse response from each particular transmitter.

[30] For a single frequency network, in which each transmitter transmits at the same frequency, the signal from each transmitter can be independently tuned, e.g. for power level and relative time delay between transmitters, so that the effects of multi-path interference are minimized in overlap areas, see area 9 in Fig. 1. At a given test station inside the overlap area, the cross-correlation functions for the various transmitters are compared, and the relative power levels of the signals from each transmitter are determined. From this information, it is possible to minimize multi-path effects by either delaying the transmission from one or more of the transmitters relative to one or more of the others, thereby maximizing the number of the signals that are received synchronously, or by adjusting the power level of one or more transmitter signals to lessen or increase their effect on the overall transmitted signal. The tuning will have minimal or no effect on the reception at various

locations outside the overlap areas, but can greatly improve the reception at locations inside the overlap areas. Preferably, the comparisons are carried out at a plurality of test stations within the overlap area, and the transmitters are tuned in such a manner as to optimize the reception throughout the overlap area.

- 5 [31] The cross correlation between $r(n)$ and $x_j(n)$ is defined by

$$\begin{aligned}
 R_{rx_j}(m) &= \sum_{n=0}^{N-1} r(n)x_j(n-m) = \sum_{n=0}^{N-1} \left\{ \sum_{i=1}^M d_i'(n) \otimes h_i + n_i(n) \right\} x_j(n-m) \\
 &= \sum_{n=0}^{N-1} \left\{ \sum_{i=1}^M [(d_i(n) + \rho x_i(n)) \otimes h_i + n_i(n)] \right\} x_j(n-m) \\
 &= \rho R_{x_j x_j} \otimes h_j + \sum_{i=1, i \neq j}^M \rho R_{x_i x_j} \otimes h_i + \sum_{n=0}^{N-1} \sum_{i=1}^M [d_i(n) + n_i(n)] x_j(n-m)
 \end{aligned} \tag{4}$$

- [32] With the orthogonal property of the selected sequence, the autocorrelation function $R_{x_j x_j}$ of the locally generated identification sequence x_j , can be approximated as a delta function. The second and third terms in the above equation (4) are only noise like sequences from the in-band DTV signals of the same transmitter and other transmitters. Therefore, the received channel response h_j from the j -th transmitter can be approximated by R_{rx_j} , i.e.

$$[33] \quad R_{rx_j}(m) = Ah_j + noise \tag{5}$$

- [34] where A is a constant determined by $R_{x_j x_j}$ and the gain coefficient ρ . The received channel response h_j from the j -th transmitter can be determined as $R_{x_j x_j}$ and ρ are known.

- 15 [35] With reference to Figure 2, the identification sequence x_i is time synchronized to the DTV signal frame structure. The illustrated signal relates specifically to an Advanced Television Systems Committee (ATSC) DTV system, but the invention is applicable to any similar system, e.g. Digital Video Broadcasting-Terrestrial (DVB-T) or Integrated Services Digital Broadcasting-Terrestrial (ISDB-T) systems.

- 20 [36] Different injection levels of the embedded identification sequence x_i are determined for ATSC, DVB-T and ISDB systems, respectively. For ATSC systems, Kasami sequences are buried

between 10 dB to 30 dB below the DTV system noise threshold, which causes negligible impact to DTV signal reception.

[37] Preferably, 16-bit Kasami sequences are used as identification sequences for a North American ATSC DTV system. However, Gold sequences and any other suitable substantially-orthogonal pseudo-random sequences may be used. The use of 16-bit Kasami sequence is a compromise of the sequence length, spreading gain and the number of the sequences, which are available for DTV transmitter identification. Figure 3 illustrates a 16-bit Kasami sequence generator, in which there are $16 + 8 = 24$ digits or $2^{24} - 1$ different initial states, which results in $2^{24} - 1$ different Kasami sequences. With reference to Figure 4, each ATSC signal data field has $312 \times 832 = 259,584$ symbols (including segment synchronization), therefore, three complete 16-bit Kasami sequences ($2^{16} - 1 = 65535$ chips) and one truncated 16-bit Kasami sequence ($2^{16} - 1 - 2519 = 63016$ chips) can be fitted into one ATSC field. The Kasami sequence chip rate should be the same as the ATSC DTV system symbol rate, i.e. 10.7622378 Msps. The Kasami sequences are injected during the transmission of the DTV data segments, but not during the ATSC DTV field synchronization transmission period to avoid interference with DTV signal acquisition.

[38] The transmitter identification process can be further reduced, if the initial values for the sequence generators only differ in the last few bits for the neighboring transmitters. By assigning different Kasami sequences this way, a blind search approach can be avoided during the transmitter identification process.

[39] Since the 16-bit Kasami sequence is very long and takes a long time to synchronize, it would be advantageous if a smaller portion of the DTV signal could be identified as a starting point, thereby facilitating synchronization. In North America the ATSC DTV field sync. PN-511 sequence, which has high signal strength, can be used as a "short code" for quick detection and synchronization of the Kasami sequence. For DVB-T and ISDB-T systems, in Europe and Japan, the cyclic prefix of the OFDM symbol can be used. Furthermore, rather than correlate the entire Kasami sequence with the received signal, the correlation function can be calculated only between the PN-511 sequence (or the cyclic prefix of the DVB-T and ISDB-T signals) and the received signal.

[40] To reduce the computation complexity during the transmitter identification process, only a desired portion of the correlation functions between the transmitted signal $r(n)$ and the local identification sequence $x(n)$ is computed. For the complete computation of the cross-correlation

between the transmitted signal $r(n)$ and the local identification sequence $x(n)$, the following equation can be used:

$$[41] \quad R(m) = \sum_{n=0}^{N-1} [r(n_0 + n + m) \cdot x(n)] \quad m = 0, 1, 2, \dots, N-1 \quad (6)$$

[42] where n_0 is the starting point of the received signal for correlation computation. For transmitter identification purposes, $R(m)$ is only needed for a length of the maximum delay spread of all the multi-path delays from all of the transmitters. In the terrestrial DTV distributed transmission case, about a 6000 DTV symbol duration or $558 \mu s$ is adequate. In fact, between $40 \mu s$ and $600 \mu s$ would suffice. This is less than 1% of the total cross-correlation function samples, which significantly reduces the computation time.

[43] Rather than conducting the correlation computation continuously in real time, a segment of the transmitted DVB-T, ISDB-T or ATSC DTV signal $r(n)$ can be separated therefrom, each of which contains one complete embedded sequence, for correlation computation.

[44] Upon synchronization of the embedded and locally generated identification sequences, using a PN511 sequence for ATSC signals or a cyclic prefix for DVB-T and ISDB-T signals, the received DTV signal can be divided into segments, each with a length of a DTV field plus two times the delay spread of the channel impulse response. Each segment begins at the starting point of each DTV field minus one delay spread and ends at the stopping point of the DTV field plus one delay spread. A sliding window technique can then be used to select portions of the transmitted signal for calculating the correlation function. The length of the sliding window is identical to one DTV field. As the window slides over the signal segment, the local identification sequence $x_j(n)$ is correlated to the received signal portion, which falls into the sliding window.

[45] Time-domain averaging is a technique used to reduce the in-band ATSC DTV signal interference. Post processing using ensemble averaging over several cross-correlation functions can improve the dynamic range of the cross-correlation function, as in Figures 6a and 6b. Several segments are correlated and an average is taken to cancel out noise distinctive of each segment and to improve resolution. Averaging improves the capability of the detection of co-channel interference and the dynamic range of the impulse response. To reduce the synchronization error effect and to optimize the superimposition of the correlation functions, prior to averaging, the peaks in each correlation function are aligned in amplitude and phase.

[46] With reference to Figure 7, due to a 6/7/8 MHz DTV bandwidth limit, each impulse in the cross-correlation function is in the form of a $\sin(x)/x$ function rather than a delta function. A first sidelobe, about 17dB below the main lobe, could be misidentified as a multi-path reflection, especially when close-in echoes exist. Post processing, or filtering using an appropriate filter response, over the cross-correlation function can reduce the side lobe of the $\sin(x)/x$ function to a negligible level, see Figure 8. One possible way to resolve the band-limitation problem is to eliminate the shape of the non-ideal auto-correlation function from the preliminary channel estimation results. To simplify the notations, the correlation result is written as: $R' = Ah + \text{noise}$ (7)

[47] Where h is the ideal impulse response to be estimated and R' is the correlation function with a truncated length L' .

$$[48] \quad R' = [R(1), R(2), \dots, R(L')]^T \quad (8)$$

[49] Where A is determined from the side lobe matrix

$$[50] \quad A = \begin{bmatrix} R_{ww}(L), & R_{ww}(L-1), \dots & R_{ww}(1) \\ R_{ww}(L+1), & R_{ww}(L), \dots & R_{ww}(2) \\ R_{ww}(L+2), & R_{ww}(L+1), \dots & R_{ww}(3) \\ \vdots & \vdots & \vdots \\ R_{ww}(L+L'-1), & R_{ww}(L+L'-2), \dots & R_{ww}(L) \end{bmatrix}$$

[51] when noise is Gaussian noise, h can be resolved using:

$$[52] \quad h = (A^H A)^{-1} A^H R', \quad (9)$$

[53] By inverting the amplitude of the embedded Kasami sequence, one-bit information can be transmitted per Kasami sequence or several Kasami sequences can be used to represent one bit, depending on the injection level of the Kasami sequence. At the receiver, a positive correlation would indicate a '1' and a negative correlation would indicate a '0'. This technique can be used to transmit low speed data over the entire DTV coverage area to provide data service or for cue and control.

[54] DVB-T and ISDB-T DTV system transmitters can also can be identified using a 12-bit Kasami sequence. The Kasami sequence should be locked to the FFT block for fast synchronization.

[55] In a distributed transmission environment, if a receiving site can identify more than three transmitters, and the transmitter geographical locations as well as their DTV transmission time delays are known, the receiving location can be calculated from the differences in arrival time of the Kasami sequences. Assuming the receiver already knows the relative position of the various transmitters, as
5 the receiver identifies the transmitter of origin of a given signal, the receiver software will be able to calculate the relative time delay between the various received signals, i.e. direct combined transmissions $d_i'(n)$. From this information the receiver processor can calculate the position of the receiver relative to the transmitters.